

# Turnout Design: Wheel/Rail Contact, Kinematic Geometry and Maintenance

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Interaction**



# Presentation Outline

## ◆ Progress on performance metrics

- Safety, Reliability, Efficiency, Capacity

## ◆ Technical progress

- Alignment Design
- Running Surface Profiles
- Transitions
- Maintenance

## ◆ Future work

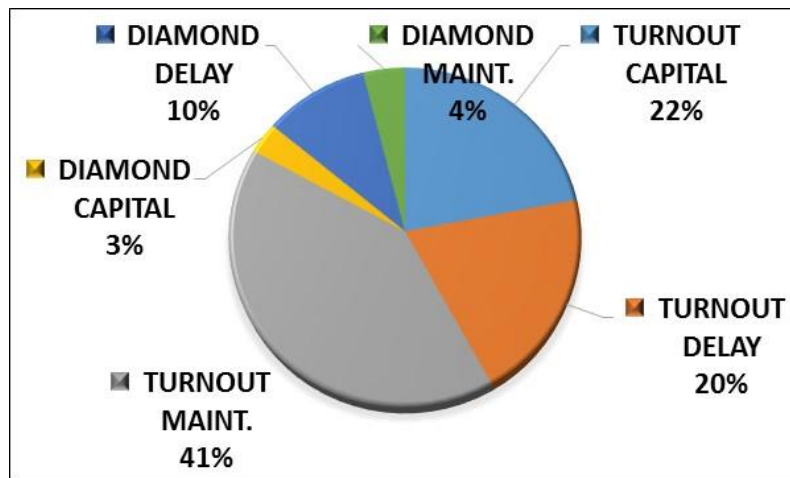


# High Performance Special Trackwork

## ◆ Problem definition:

- Special trackwork costs more than \$1B/year
- Maintenance and train delay more than half of total costs
- Dynamic load-sensitive components
- Frog & switch point lives increasing
  - Still less than half of that of surrounding rail
- Fatigue failures still significant
- Running surface profile maintenance increasing

Distribution of Special Trackwork Costs



Source: TTCl analysis of R-1 data



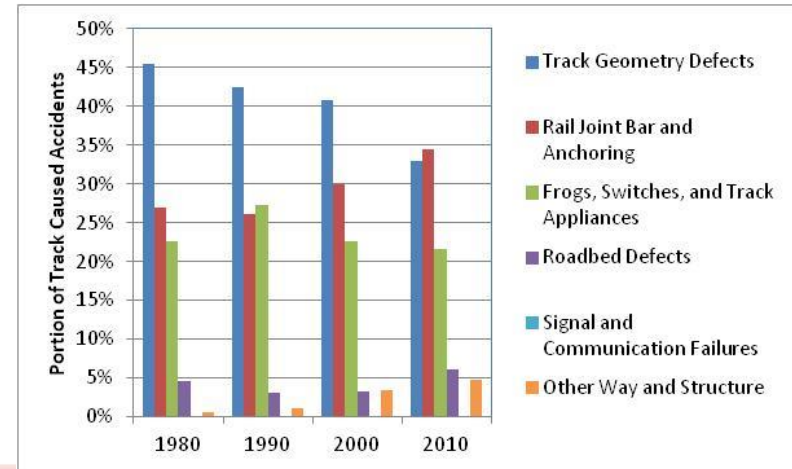
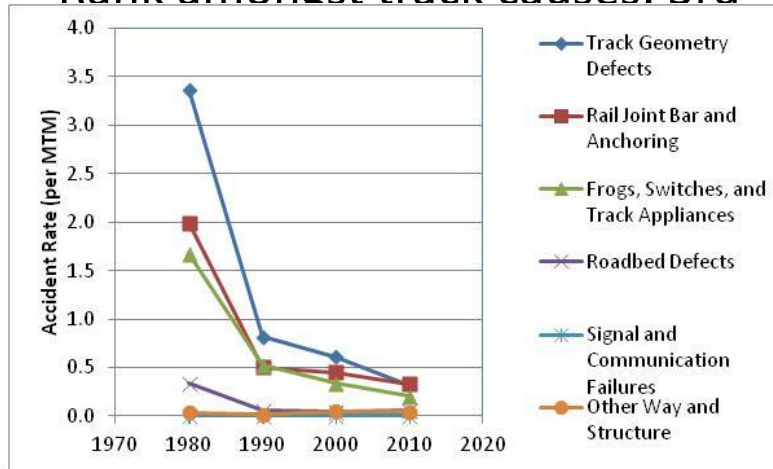
# HAL Key Track Technology Enablers

- ◆ **HAL special trackwork performance (1980 – 2010)**
- ◆ **Improved service lives (from AAR Project audit)**
  - Turnout life: 500 MGT – 2,000 MGT
  - Frog Life: 100 MGT – 500 MGT
  - Diamond Life: 10 MGT – 100 MGT
- ◆ **Reduced accident rates (TTCI analysis of FRA safety database)**
  - Rate reduction: 88% Reduction since 1980
  - Rank amongst track causes: 3rd – 3rd
- ◆ **Reduced turnout maintenance (FAST experience)**
  - Labor hours per MGT:
    - 2.07 hrs/MGT 1980s
    - 0.58 hrs/MGT – today
    - 77% reduction



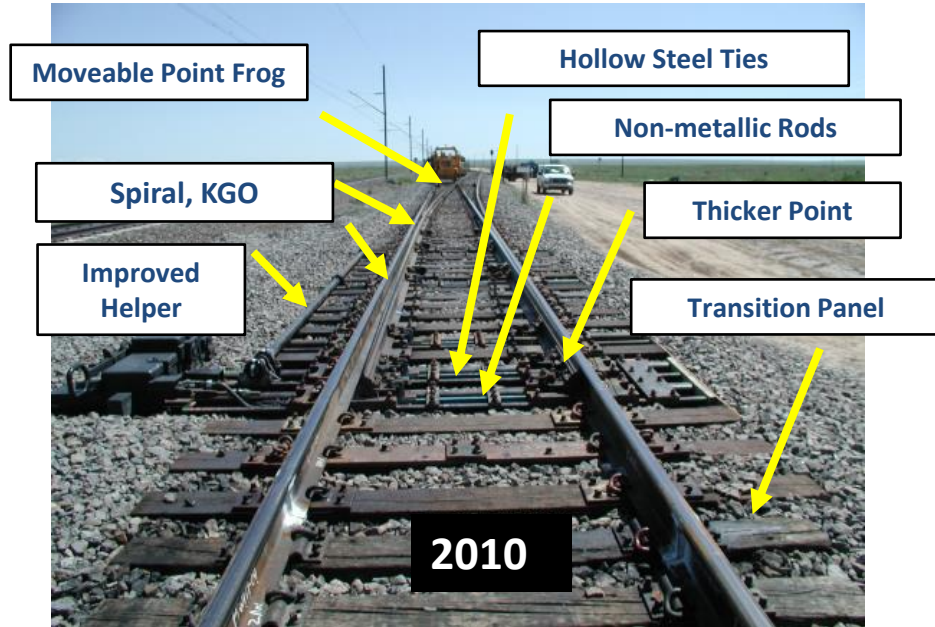
# HAL Key Track Technology Enablers

- ◆ HAL special trackwork performance (1980 – 2010)
- ◆ Reduced accident rates (TTCI analysis of FRA safety database – Class 1 railroads)
  - Rate reduction: 88% reduction since 1980
  - Rank amongst track causes: 3rd – 3rd



# HAL Key Track Technology Enablers

- ◆ Subtle, but significant changes.



# Improved Special Trackwork

- **Areas of Improvement**

- Alignment Design\*

- Compromise between dynamic performance and service life

- Running Surface Profile Design\*

- Make profiles near conformal

- Transitions

- Track structure change effects can be minimized\*

- Maintenance

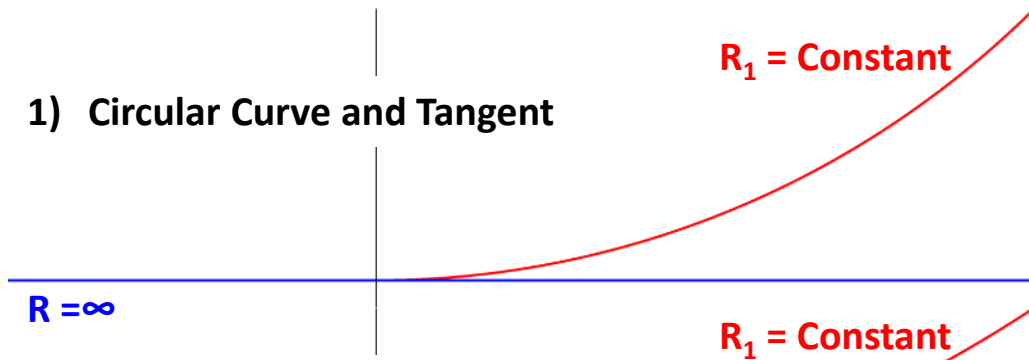
- Accessibility to minimize track time

\*We have the design tools to make significant improvements

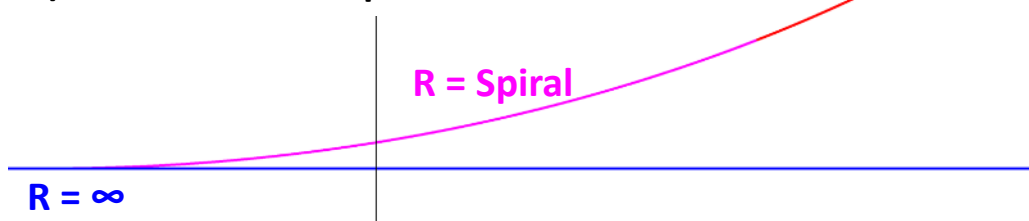


# Track Layout “101”

## 1) Circular Curve and Tangent



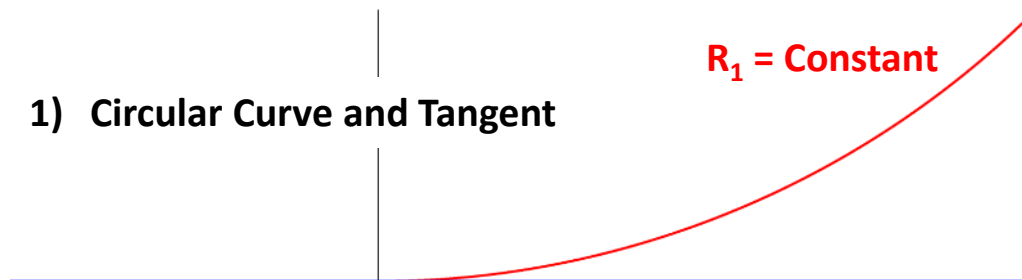
## 2) Add Transition Spiral



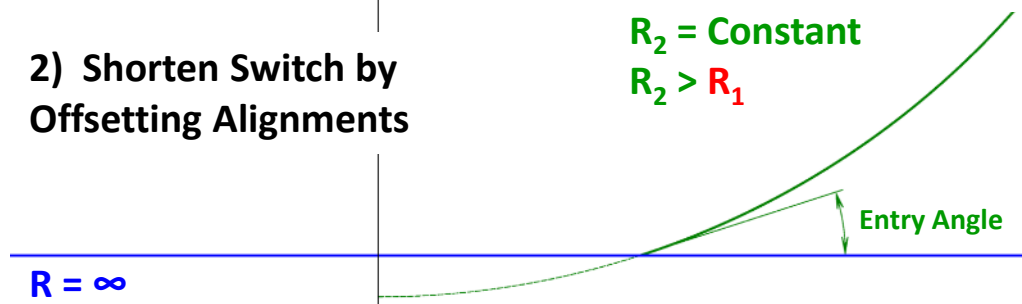


# Turnout Layout “101”

## 1) Circular Curve and Tangent

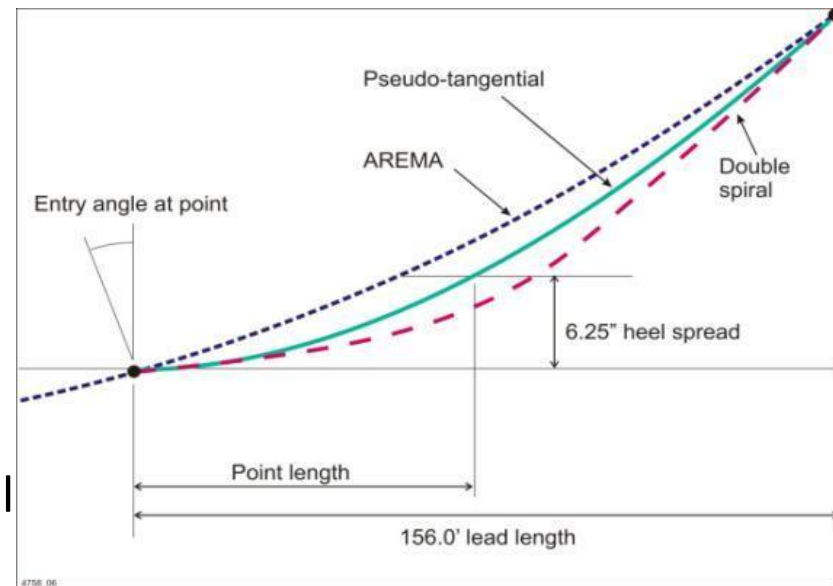


## 2) Shorten Switch by Offsetting Alignments



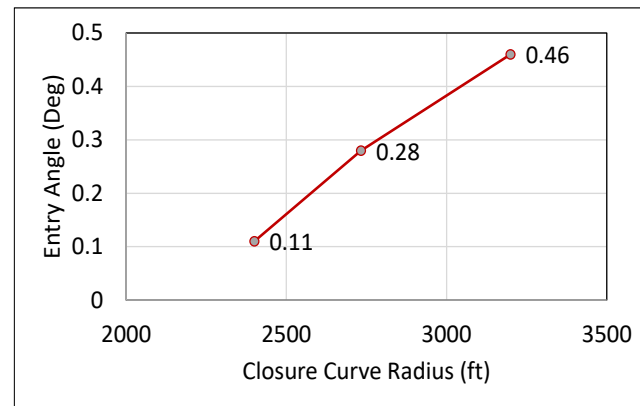
# Alignment Design: Smoothing Alignments

- **Under current allowable speed rule:**
  - Maximize closure curve radius
    - High entry angle and forces near point of switch
- **Proposed:**
  - Balance entry and curving forces
    - Pseudo-tangential
    - Double spiral
    - Add elevation to compensate for small radius curve
  - Modify cant deficiency rule



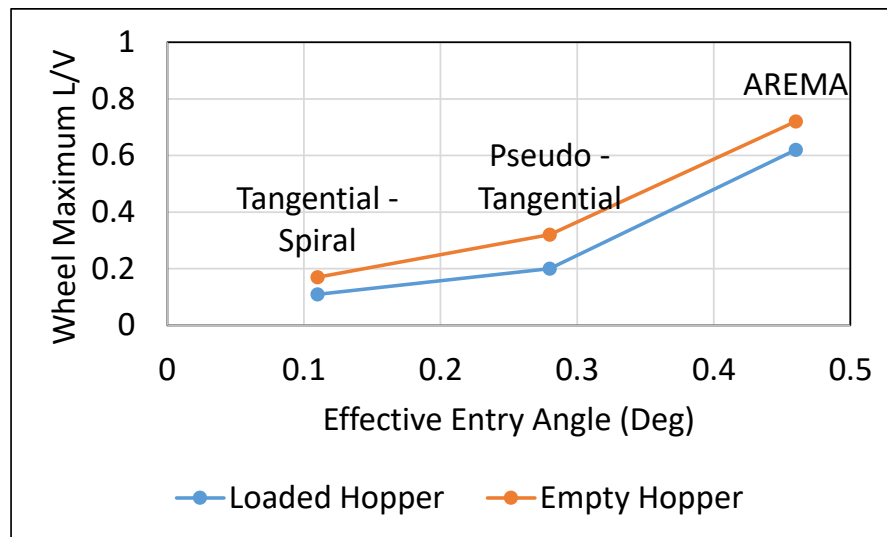
# Turnout Geometry Design: North American Benchmarking

- **Comparison of #20 turnout alignments for predicted dynamic loads**
  - study assumed a fixed turnout length 47.5 m (156 ft.)
- AREMA style (non-tangential) alignment
  - Large entry angle, circular curves
- Pseudo-tangential (low entry angle) alignment
  - Straight cut, circular curves
- Tangential – spiral alignment
  - Spiral to spiral
- Entry angle – closure curve radius trade-off



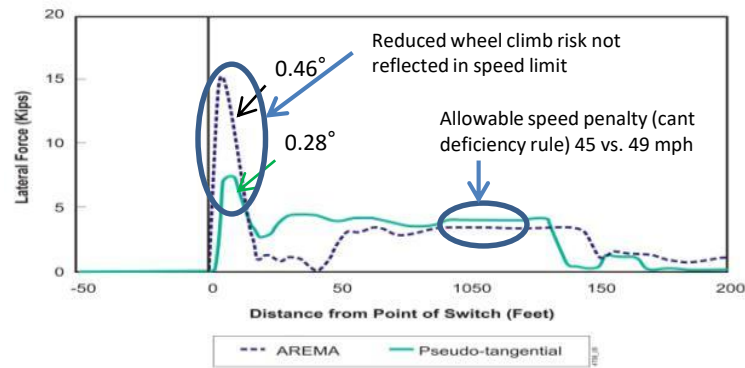
# Turnout Geometry Design: North American Benchmarking

- Comparison of #20 turnout alignments for predicted dynamic loads — study assumed a fixed turnout length 47.5 m (156 ft.)
  - AREMA style alignment
  - Pseudo - tangential (low entry angle) alignment
  - Tangential – spiral alignment
    - Predicted dynamic performance (NUCARS®)



# Optimized Turnout Alignment – Findings

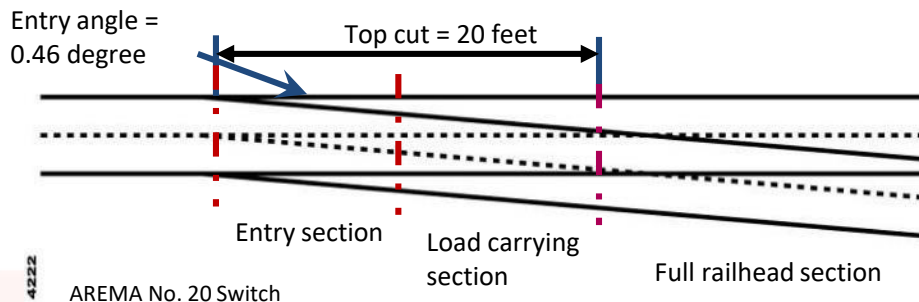
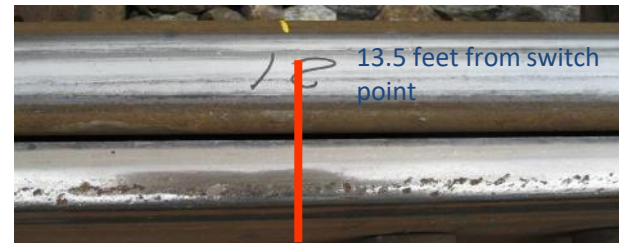
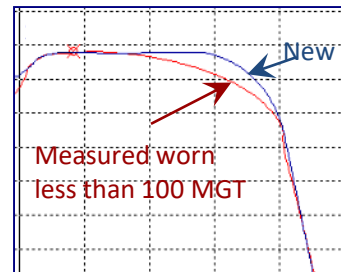
- **Minimize maximum lateral forces and life cycle costs**
  - Entry angle: significant effect
    - Pseudo-tangential alignments will provide significant benefit without lengthening switch
- **Diverging alignment: spirals important for reducing accelerations**
- **Super elevation: minimal effect on net lateral forces. Will raise allowable speed under current rule by ~5-10 mph**
- **Running surface profiles: Smooth transitions are critical**



# Switch Point Profile Design and Testing

## ◆ Findings

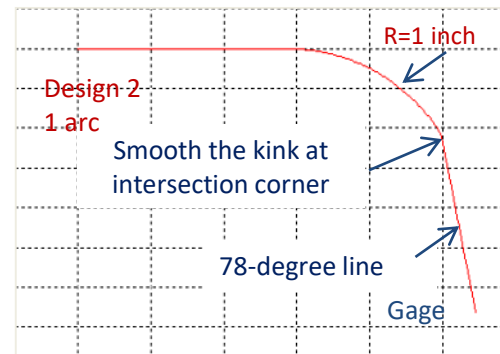
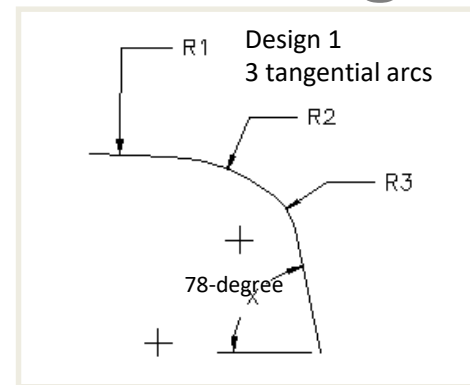
- Point profiles play significant role in formation of rolling contact fatigue (RCF)
- Point wear concentrated at the gage corner
- Severe RCF defects generally first formed within the top cut section at gage corner
- Switch points show greater RCF than the matching stock rails



# New Switch Point Profile Design and Testing

## ◆ Tests

- Two switch point profiles redesigned to improve contact conditions with anticipated reduced
  - Surface damage
  - Wear
  - Plastic flow at rail gage
- TTCI, railroads, and one supplier to build and test prototype switch point rail profile designs
  - Prototype and base to be located on same line to assure similar traffic environments for comparison



Simplify the machining process  
Utilize an existing tool



# Prototype Switch Points in Revenue Service

**BNSF – Marceline, MO**



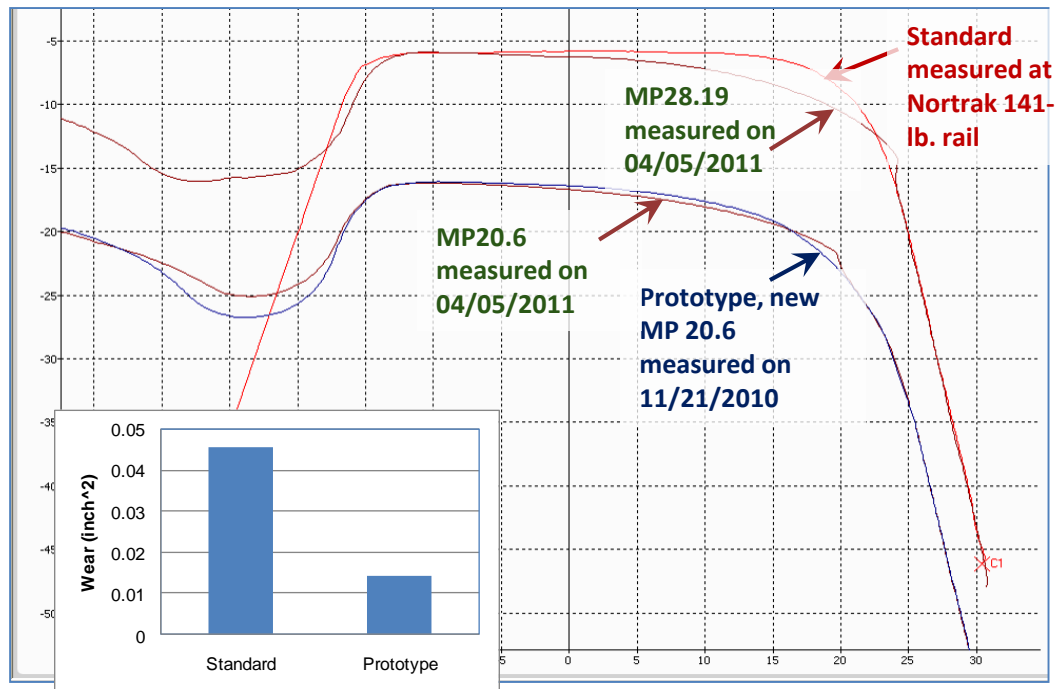
**Union Pacific – Bonner Springs, KS**





# Comparison of New and Worn Switch Point Rail Profile

Straight points @ 13 feet from p.o.s.



# New Switch Point Profile Design and Testing

**Key Findings: Initial performance of Prototype Switch Point Profiles looks promising**

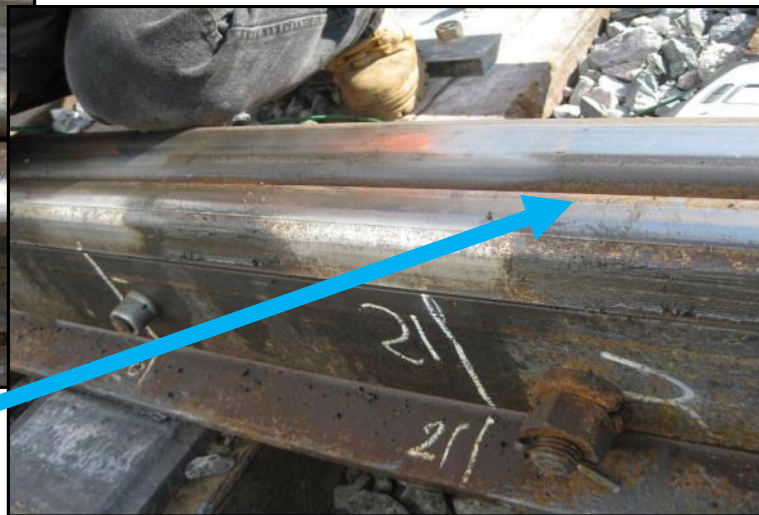
Standard Straight Point



Contact on gage corner

Contact centered

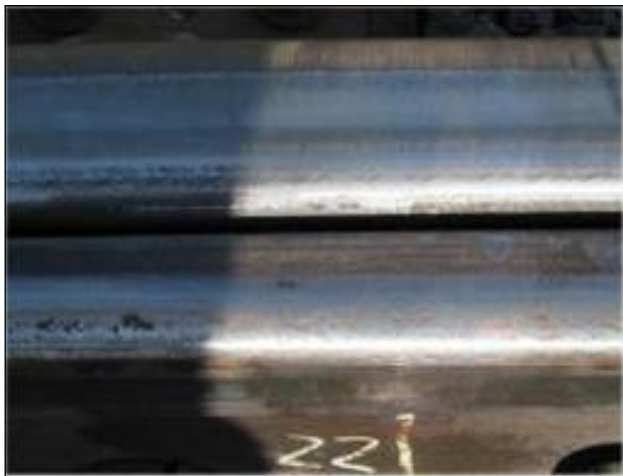
Prototype Straight Point



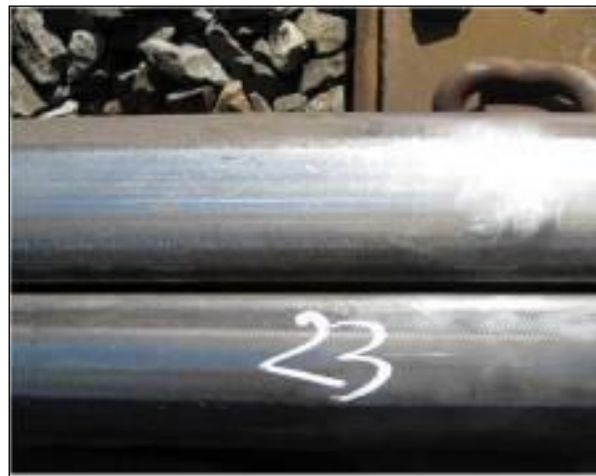
# Running Surface Appearance

## Standard and Prototype

**Straight, @ 14 and 15 ft from p.o.s.**



**Standard point – RCF present**



**Prototype point – no RCF**



# New Switch Point Profile Design and Testing

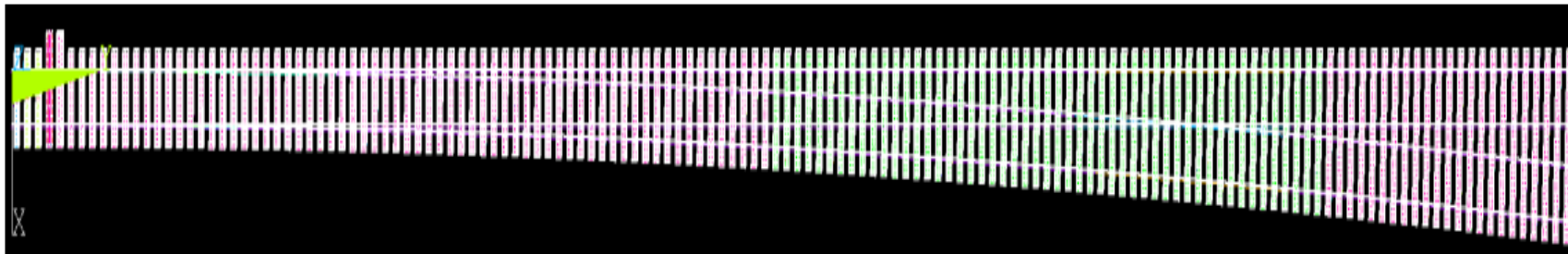
## ◆ Conclusions

- Simplified profile working as intended
  - Care should be taken to orient 1 inch radius to match canted rail
  - Significant reduction in wear (>50%)
  - Less RCF forming
- Prototypes closer to design performing better
- Study whether 3 radius design is feasible
  - 3 radius design was adopted by most railroads



# Optimize Vertical Turnout Stiffness

- ◆ **Objectives: Test prototype turnout foundations to reduce stiffness changes, dynamic loads and settlement**
  - Proof of concept test
    - Timber ties and under-tie pads
  - FAST test began 2013:
    - Canadian Pacific RR #20 Turnout with Pads 1 and 2



Pad 1 to match open  
track

Pad 2 also adds  
damping



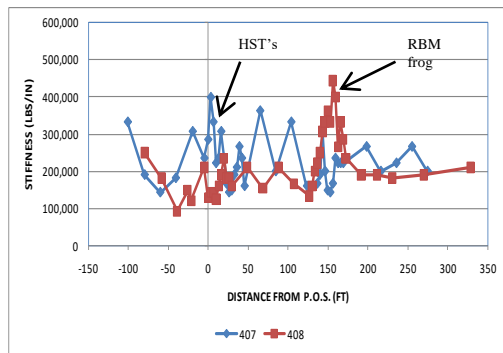
# Turnout Foundation Test

## Description of Test

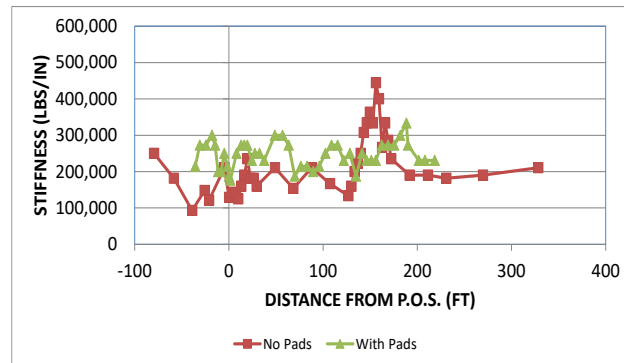
- ◆ Vertical stiffness variations due to longer ties, platework and extra rails in turnouts
- ◆ Under-tie pads installed in turnout
  - Uniform stiffness 200,000 – 250,000 lbs./in.



#20 Turnout With Under-tie Pads



#20 Turnouts Stiffness measured at  
FAST HTL – No pads



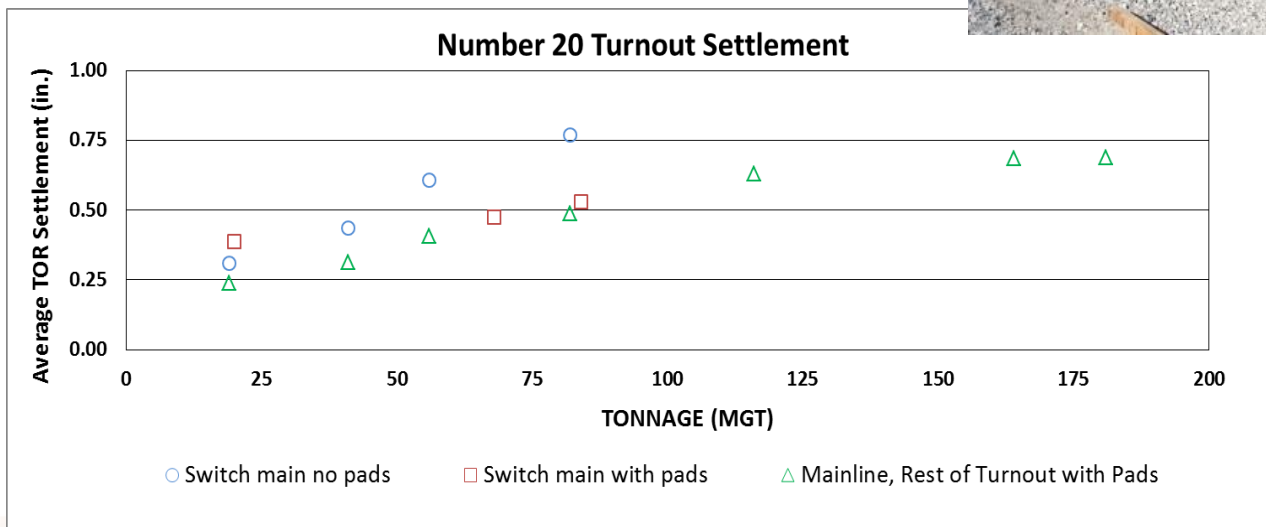
#20 Timber Tie Turnouts with RBM Frogs



# Turnout Foundation Test

## Preliminary Results

- ◆ Uniform stiffness 200,000 – 250,000 lbs./in.
- ◆ Reduction in settlement by ~33%
- ◆ More uniform settlement



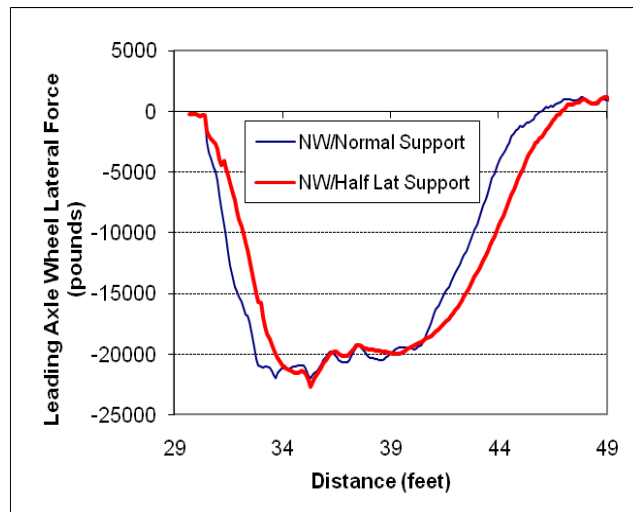
# Optimize Lateral Stiffness of Switch

## ◆ Traditionally, lateral stiffness in switch is made as high as practicable

- Safety
- Creates a “hard spot” in the track

## ◆ Dynamic simulations show that there is an effect of lateral stiffness on maximum forces

- An optimal range of lateral stiffness may exist where forces are lower and safety is not compromised
  - Contact occurs later in switch (switch point is thicker)
  - Empty car forces should also be reduced





# Optimize Lateral Stiffness of Switch



**FAST Testing**

## ◆ Effects of Lateral Stop Stiffness on Turnout Forces Preliminary Conclusions:

- Lateral stiffness of switch point stop can reduce facing point lateral forces 10-15%
- Relatively low-cost modification can make a marginal improvement in performance
- Turnout footprint is often a rigid constraint
  - Can be applied to large entry angle switches

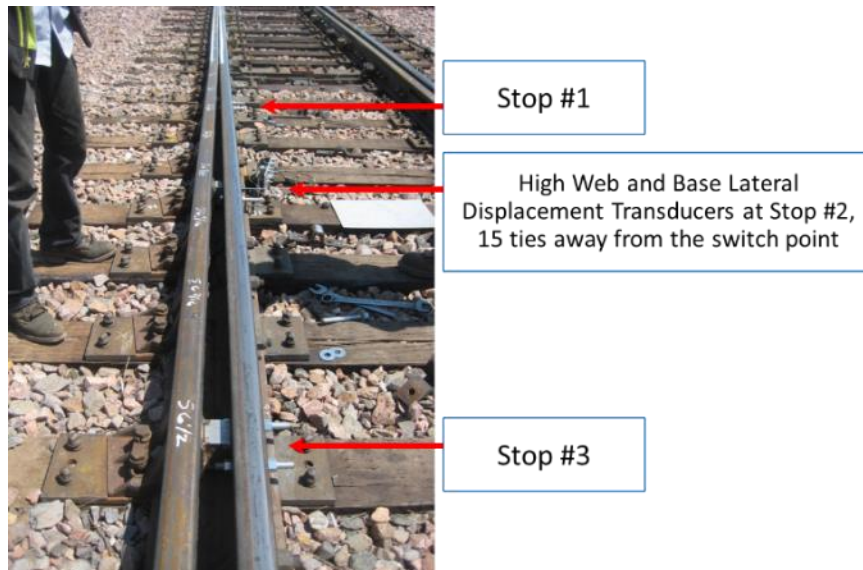


# Compliant Switch Evaluation

## FAST Testing

### ◆ Effects of Lateral Stop Stiffness on Turnout Forces

- Six variations of switch point stops
- Quantify lateral forces, L/V ratios, and rail displacements



# Compliant Switch Evaluation

## FAST Testing:

### ◆ Lateral Stops Evaluated (2 of 6):



Standard Stop



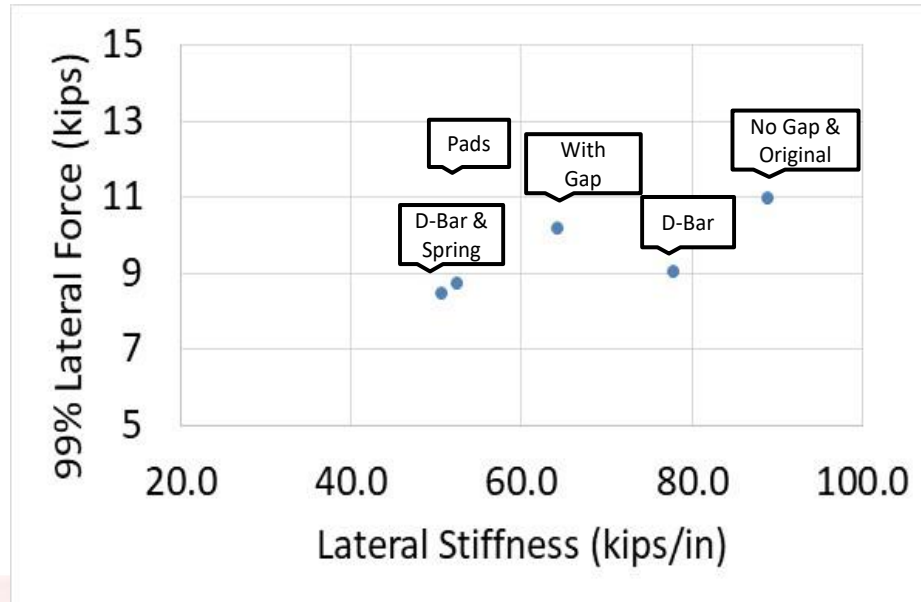
Spring Stop: D Bar contact



# Compliant Switch Evaluation

## FAST Testing

- ◆ **Effects of Lateral Stop Stiffness on Turnout Forces**
  - Six variations of switch point stops



# STW – Advanced Designs & Materials

- ◆ **Key findings: Turnout maintenance under HAL**
- ◆ **Comparison of FAST maintenance effort 1980s to today**
  - Significant improvement in Labor Hours/ MGT

FAST Turnout	Turnout Maintenance (hr/MGT)	Component Replacement (hr/MGT)	Total Maint & Replacement (hr/MGT)
1980s T.O.	1.42	0.65	2.07
1990s T.O.	0.85	0.19	1.04
2000 AREMA T.O.	0.55	0.07*	0.63
2010 T.O.s	0.33	0.27	0.60

\* Major component failure shortened turnout life and reduced component replacements



# STW – Advanced Designs & Materials

- ◆ **Key Findings: Turnout Maintenance under HAL**
  - Biggest decrease in Turnout Maintenance hours
    - All fasteners accessible from the top (e.g. capture blocks)
    - Initial worn shapes reduce initial grinding required
    - Better dynamic performance has extended component life
  - General trend: running surface maintenance is taking a larger share of total maintenance
    - Other maintenance is decreasing due to lower dynamic loads



# Turnout Design

## ◆ Future Work:

- Vertical switches
  - For low volume, low speed diverging traffic
  - Eliminate running surface discontinuities for mainline route
- Frog materials
  - Reduce metal flow and fatigue cracking
  - Needed to improve Flange Bearing Frogs economics



# Turnout Design

## ◆ Future Work (2):

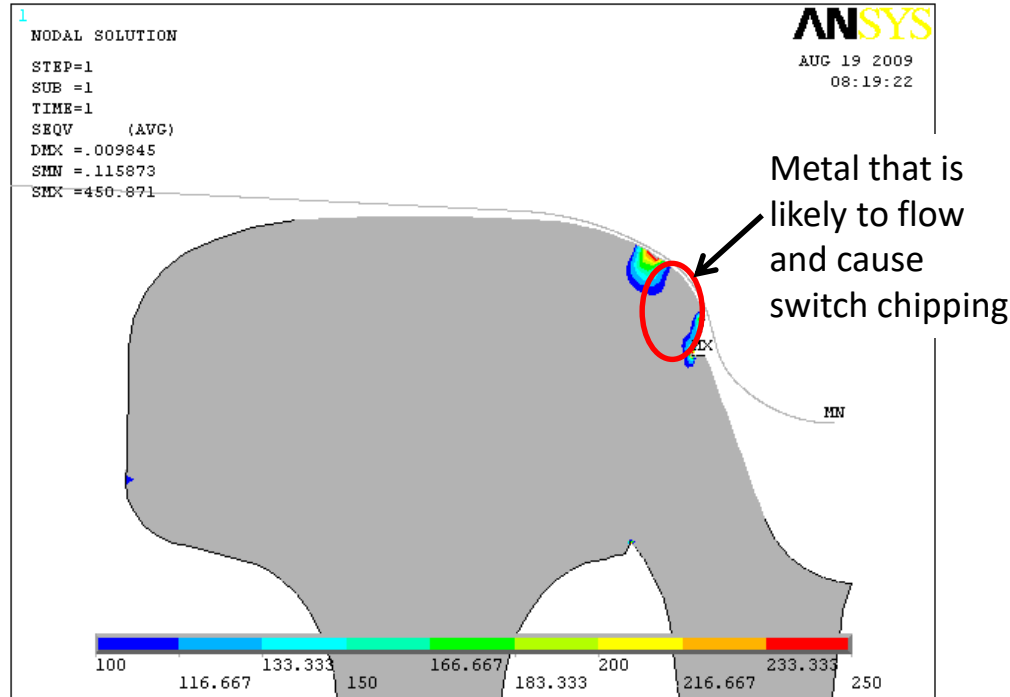
- Rail running in turnouts
  - Better handling of rail longitudinal forces
- Switch point fatigue
  - Redesign switch point- stock rail interface
    - » Stock rail flow and switch point twist create adverse contact





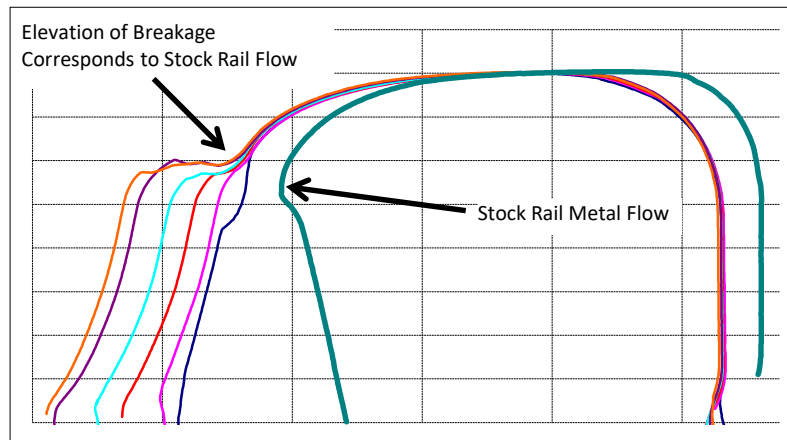
# Future Work: Prevent Switch Point Chipping

## ◆ Stock Rail Flow Leads to Switch Point Chipping



# Switch Failure Modes Analysis

- ◆ **Key Findings: Stock Rail/ Switch Point fit should be more robust**
- ◆ **Field survey**
  - Common height for chipped out points — indicates stock rail flow contact





## TTCI Special Trackwork Team

- Ben Bakkum
- Duane Otter
- Steve Wilk
- Bea Rael
- Joseph LoPresti
- Xinggao Shu
- Charity Duran
- Don Guillen
- Rafael Jimenez
- Dave Davis

**Thank you for your kind attention**